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## ULTRASONIC, ULTRAVIOLET, AND HYBRID CATALYTIC PROCESSES FOR THE DEGRADATION OF RHODAMINE B DYE: DECOLORIZATION KINETICS

### PROCESOS CON RADIACIÓN ULTRASÓNICA, ULTRAVIOLETA Y CATALÍTICOS HÍBRIDOS DURANTE LA DEGRADACIÓN DEL COLORANTE RODAMINA B: CINÉTICA DE DECOLORACIÓN

J.A. Ayala, C.O. Castillo, R.S. Ruiz\*

Grupo de Procesos de Transporte y Reacción en Sistemas Multifásicos, Depto. de IPH, Universidad Autónoma Metropolitana -Iztapalapa, Av. San Rafael Atlixco No. 186, C.P. 09340, México D.F., Mexico. Received November 30, 2016; Accepted February 3, 2017

#### Abstract

The degradation of Rhodamine B dye was evaluated under different radiation conditions: sonolysis, photolysis, sonocatalysis, photocatalysis, and sonophotocatalysis, where commercial  $TiO_2$  was utilized as catalyst. Color removal was monitored by spectrophotometry and mineralization was determined by TOC analysis. A two-first-order in-series reactions model was developed; it takes into consideration reaction times where the intermediates prevail. In this reaction scheme, the first reaction is the degradation of the coloured dye into coloured intermediates, and the second reaction is the conversion to colorless products. Good agreement was observed between experimental data and the developed kinetic model. The results suggest that dye degradation rate is more than one order of magnitude larger than the corresponding one for coloured degradation of intermediates. Under experimental conditions considered, water-soluble materials predominated over mineralized products within colorless products.

Keywords: synthetic dye, sonocatalysis, photocatalysis, hybrid process, kinetics.

#### Resumen

La degradación de la Rodamina B se evaluó bajo diferentes condiciones de radiación: sonólisis, fotólisis, sonocatálisis, fotocatálisis y un proceso híbrido de sonocatálisis y fotocatálisis, donde se utilizó TiO<sub>2</sub> comercial como catalizador. El seguimiento de las reacciones de degradación y mineralización de Rodamina B se llevó a cabo mediante espectrofotometría y análisis de carbón orgánico total (TOC), respectivamente. Se desarrolló un modelo cinético que considera un esquema de reacción en serie. El proceso hibrido presentó la mayor tasa de degradación y mineralización. En este esquema de reacción en serie, la primera reacción es la degradación del colorante a intermediarios orgánicos con color, y la segunda reacción es la degradación de degradación de compuestos con color es mayor que la velocidad de degradación de compuestos con color es mayor que la velocidad de degradación de compuestos sin color. A las condiciones de estudio evaluadas en este trabajo, la concentración de productos formados por el mecanismo de degradación de rodamina B a productos solubles en agua, fue mayor que la concentración de productos formados por el mecanismo de mineralización, óxidos de carbono, sales y agua.

Palabras clave: colorante sintético, sonocatálisis, fotocatálisis, proceso híbrido, cinética.

## **1** Introduction

Textile industry is in general one of the most water polluting industries, and it is estimated that around 10 to 20% of dyes are lost in the dyeing section of the industry due to process inefficiencies. Dyestuff in effluents disposed to water bodies imparts color and toxicity that are undesirable and harmful to the environment because of their refractory and carcinogenic nature (Barka *et al.*, 2011). The presence of one or several benzene rings in the dye structure makes them highly stable molecules that are difficult to degrade by conventional chemical and biological methods (Pang *et al.*, 2010). Therefore, several

<sup>\*</sup> Corresponding author. E-mail: rmr@xanum.uam.mx

methods based on advanced oxidation processes such as photolysis, sonolysis and electrochemistry, have been developed for the removal of these pollutants from effluents by using hydroxyl radicals to degrade and mineralize the organic compounds (Aguilar *et al.*, 2014; Barka *et al.*, 2011; Pang *et al.*, 2010; Priya *et al.*, 2006; Tezcanli-Guyer and Ince, 2004).

Photocatalytic treatment has been considered as an attractive alternative for water treatment and mineralizing organic compounds to carbon dioxide, water and mineral acids (Pantoja-Espinoza et al., 2015; Moctezuma et al., 2016). In particular, the easy synthesis of TiO<sub>2</sub> and its semiconducting properties leading to high photoactivity make this material one of the most used to mineralize recalcitrant organic molecules (Ding et al., 1999; Saggioro, et al., 2011). However, some recent studies suggest the convenience of using combined or sequential methods over a single technique, i.e. process intensification. For instance, the combined operation of photocatalysis with sonolysis seems to enhance the photocatalytic efficiency and a synergetic effect between both technologies (Ertugay and Acar, 2016; Wu et al., 2014; Mathivanan et al., 2016). Both of these techniques, photocatalysis and sonolysis, have the potential of degrading dye molecules via OH attack. If the two radiation modes (UV and ultrasound) are operated in combination, a greater number of free radicals will be available for the reaction thereby increasing the rate of reactions. Equations (1) to (7) are typical of photocatalysis and Equation (9) denotes the contribution of ultrasound to radical formation, which can be extrapolated to sonocatalysis. In the case of sonolysis, ultrasound induces electrohydraulic cavitation in water and by which generated gas bubbles can implode violently generating local extreme conditions (5000 K and 1000 atm) under which water molecules readily disassociate as described by Eq. (9) (Priya and Madras, 2006). Furthermore, other possible reasons for the synergic effect between photocatalysis and sonocatalysis can be expected to include dispersion of aggregates of catalyst particles, refreshing of the TiO<sub>2</sub> surface, enhancement of mass transport, and pyrolysis in cavitation bubbles produced by ultrasound (Mathivanan et al., 2016).

$$TiO_2 + hv \to TiO_2(e^-) + TiO_2(h^+) \tag{1}$$

$$H_2 O \to O H_{ads}^- + H^+ \tag{2}$$

$$h^+ + OH^-_{ads} \to OH \tag{3}$$

$$e^- + O_2 \to O_2^{--} \tag{4}$$

$$H^+ + O_2 \to HO_2^{\cdot} \tag{5}$$

$$H^{+} + O_{2}^{\cdot -} + HO_{2}^{\cdot} \to H_{2}O_{2} + O_{2}$$
 (6)

$$H_2O_2 + hv \to 2^{\circ}OH \tag{7}$$

$$OH + OH \to H_2O_2$$
 (8)

$$H_2O+))) \to OH + H \tag{9}$$

Dye degradation and mineralization by OH attack is a gradual process that involves a series of reactions that generate several intermediate products. For instance, in studies on the photocatalytic degradation of Rhodamine B up to 25 different intermediate color and colorless products have been reported in the mineralization process (He et al., 2009; Natarajan et al., 2009). In this sense, understanding the kinetics of dye degradation under ultrasound and/or ultraviolet radiation processes seems essential to achieve higher efficiencies. In this regard, kinetic studies have been reported for diverse photocatalytic and sonocatalytic systems (e.g. Barka et al., 2011; Ding et al., 1999; Pang et al., 2010; Priya et al., 2006; Moctezuma et al., 2016; Tezcanli-Guyer and Ince, 2004; Saggioro, et al., 2011). For these systems literature studies have often presented their results in terms of first-order or Langmuir-Hinshelwood (L-H) kinetic models. This approach, however, focuses mainly on the degradation of a dye molecule. On this regard, kinetic analysis accounting for sequential reaction steps appears to be comparatively scarce and, to the best of our knowledge, it has not been reported previously for describing the hybrid process between photocatalysis and ultrasonically assisted catalysis, hereafter called sonophotocatalysis.

In the present work a model molecule, Rhodamine B basic dye, was degraded under different radiation conditions based on ultrasound and ultraviolet light and their combination. Ultrasonic, sonocatalytic, and sonophotocatalytic reaction results are then interpreted in terms of a two first-order in series reaction model that contemplates initial dye degradation into intermediate dyes and the further degradation of the latter into colorless material, which include both water-soluble molecules and mineralized products. The effect of the different operating conditions considered on reactor performance was discussed in terms of the variations observed in the relative magnitudes between the kinetic constants for dye and intermediate decomposition reactions, respectively.

## 2 **Procedures**

Rhodamine B purchased from J.T. Baker (99.8% purity) and distilled water were used in all the cases to prepare the desired concentration of the dye in the solution. Titanium dioxide (Degussa P-25) was used, when required, as catalyst. It had an average particle size of 30 nm and specific surface area of 55 m<sup>2</sup>/g. The anatase and rutile percentage was 80 and 20% respectively.

Experiments were conducted in a 2.7 L thermostatic cylindrical Pyrex vessel, open to air, containing 1.0 L of the solution. In each experiment 30 mg  $L^{-1}$  RhB solution containing a previously determined optimum concentration of titanium dioxide (1.0 g  $L^{-1}$ ) was sparged with air at a flow rate of 2.4 L min<sup>-1</sup> (Alvarado-Camacho *et al.*, 2014). An ultrasonic direct-immersion horn sonicator (Cole-Palmer TM), 20 kHz, 500 W, fitted with a 25 mm diameter probe, was utilized for generating ultrasonic sound waves in the reactor. The reaction vessel was also equipped with two 6 W ultraviolet lamps (with a maximum peak of 350 nm, 0.20 m long with 0.013 m diameter) which were immersed in axial position inside the reactor opposite two each other. The setup used herein is shown in Fig. 1. To control the reactor temperature at the selected value of 25°C  $(\pm 2 \, ^{\circ}\text{C})$  cold water from a thermostatic bath was pumped through the reactor jacket. The reactor was operated either under sonication, UV radiation, or under the combination of both modes of energy radiation. Samples were withdrawn from the reactor and centrifuged immediately for separation of the suspended solids with a centrifuge CHE SCIENTIFIC I, HKSC-220. All experiments were performed in triplicate and the average values are reported.

The remaining amount of Rhodamine B at a given time was determined by UV-vis spectroscopy. Every solution sample was analyzed for its absorbance at 554 nm using a HACH DR 6000<sup>TM</sup> UV VIS Spectrophotometer with RFID Technology. The absorption was converted to a concentration through a calibration curve obtained using known concentration solutions of RhB using the Beer-Lambert law. Furthermore, mineralization of Rhodamine B solution was quantified from the decrease of total organic carbon. TOC was determined with a HACH DR200 Spectrophotometer, by means of HACH direct method 10129 for low range concentrations (0-20  $mgL^{-1}$ ). In this method total organic carbon standard solutions at known concentrations were used to obtain a calibration curve. Analysis of degradation and



Fig. 1. Schematic diagram of experimental set-up. mineralization were performed in triplicate.

## **3** Results and discussion

#### 3.1 Ultraviolet (UV) degradation

Rhodamine B degradation profiles under ultraviolet conditions are shown in Fig. 2 for the following cases: i) in the absence of catalyst; ii) in the presence of catalyst; and iii) in the presence of both catalyst and ultrasonic radiation. As expected the photolysis alone appears to be the lowest efficient method of degradation among the three cases considered. In this regard, although dye degradation was favored by the presence of TiO2 catalyst under photocatalytic conditions, larger degradation rates appear to occur under photosonocatalytic conditions. Although relatively small, the UV light had evident contribution on the dye degradation as also observed by other researchers (Natarajan et al., 2011; Tseng et al., 2011). The difference between direct photolysis and photocatalysis suggests that UV and TiO<sub>2</sub> photocatalyst have a synergic effect on the degradation of RhB. Since OH radicals are considered to be the dominant oxidizing species contributing to the photocatalytic degradation of organic substrates,



Fig. 2. Decolourization profiles of RhB solution under UV light radiation in the absence of catalyst, in presence of catalyst, and in presence of catalyst and in combination with ultrasound.



Fig. 3. Decolourization profiles of RhB solution under ultrasound in absence of catalyst, in presence of catalyst, and in the presence of catalyst in combination with UV light radiation.

dye degradation can be primarily associated to the generated OH radicals. Also shown in Fig. 2 is the degradation of rhodamine B for the case in which the catalytic system was simultaneously exposed to UV light and ultrasonic (US) radiation. It is clear that larger dye degradation rates were obtained for the UV/US/TiO<sub>2</sub> system in comparison with the UV treatments. The reason for this is that the basic mechanism for both ultrasonic and photocatalytic oxidations is the generation of free radicals. It is known that ultrasound waves with frequencies greater than 16 kHz can produce acoustic cavitation in water. The heat generated locally from the cavity implosion decomposes water and then highly reactive species are formed such as hydroxyl ('OH), hydrogen ('H), hydroperoxyl ('HO<sub>2</sub>) radicals and hydrogen peroxide, which can readily react and degrade organic compounds (Joseph *et al.*, 2009). Therefore, if these modes of radiation (UV and US) are operated in combination, an increase of the rate of reaction can result mainly from a larger number of radicals available for the reaction, nevertheless, a synergetic effect can also occur as ultrasound has been reported to enhance mass transport, catalyst particles dispersion, and refreshing of the TiO<sub>2</sub> surface.

#### 3.2 Kinetics

Many researchers have reported that sonochemical degradation can be fitted to pseudo-first order kinetics (Behnajady et al., 2008; Inoue et al., 2006; Okitsu et al., 2005; Wang et al., 2003) or to Langmuir-Hinshelwood (L-H) type of models (Chiha et al, 2010; Merouani et al., 2010; Okitsu et al., 2005). Likewise, it has also been suggested pseudo-first order kinetics for sonocatalytic and photocatalytic degradation of dyes (Goel et al., 2004; Vinu and Madras, 2009; Pang et al., 2010b; Kavitha and Palanisamy, 2011; Joseph et al., 2012) or to L-H kinetic-type of models (Barka et al., 2011; Priya and Giridhar, 2006; Wu et al., 2014). In most of the reports discussing the first-order reaction kinetics, a simple semi logarithmic plot of log[C] (or ln[C], ln[C]/[C0], etc.) vs. time has been often used, and the information obtained is roughly analyzed to obey a pseudo-first order kinetic model (Okitsu et al., 2005). In the case of the studies that employ L-H type models have been limited to describe initial concentration changes. It can be expected, however, that reaction conditions change with time because products formed can scavenge generated 'OH radicals, and, hence, reported models may not be valid in longer reaction times where the effect of intermediate products prevail (Ghows and Entezari, 2013). Therefore, in the present work a kinetic approach that not only considers reaction of the original component, but also that of the intermediate products has been utilized, as depicted by Eq. (10), and in which the system is modeled by two first-order in-series reactions as suggested by other researchers (Ghows and Entezari, 2013; Julson and Ollis, 2006; Bergamini et al., 2009).

# $dyes \xrightarrow{k_1}$ intermediates $\xrightarrow{k_2}$ colorless products (10)

The sonolityc color removal data is presented in Fig. 4a in a semi log plot. It appears from this plot that a single straight line does not fit the data for the entire period of radiation, and instead two regions (dashed lines) can be identified that suggest a two first-order inseries reactions. Under these circumstances, assuming

that both reactions are first-order, eqs. (11) and (12) can describe the change of the concentrations with time of the dye and intermediates, respectively  $C_D$  and  $C_I$ , with the following initial conditions: for t = 0,  $C_D = C_{D0}$  and  $C_I = 0$ .

$$\frac{dC_D}{dt} = -k_1 C_D \quad \Rightarrow C_D = C_{D0} e^{-k_1 t} \tag{11}$$

$$\frac{dC_I}{dt} = k_1 C_D - k_2 C_I \quad \Rightarrow C_I = \left(\frac{k_1 C_{D0}}{k_2 - k_1}\right) \left(e^{-k_1 t} - e^{-k_2 t}\right) \tag{12}$$

Measured absorbance is considered to be the sum of contributions from the dye and intermediates. Therefore, eq. (13) was obtained by combining Lambert-Beer equation ( $Abs = \alpha_D C_D + \alpha_I C_I$ ) and eqs. (11) and (12), and where  $\alpha_D$  and  $\alpha_I$  are respectively the molar absorptivity of the dye and intermediates.

$$Abs_{t} = Abs_{0} \left[ \left( \frac{\alpha_{I}}{\alpha_{D}} \frac{k_{1}}{k_{2} - k_{1}} \right) \left( e^{-k_{1}t} - e^{-k_{2}t} \right) + e^{-k_{1}t} \right]$$
(13)

A nonlinear least-square algorithm (Levenberg-Marquardt) was applied to the experimental absorbance data to fit eq. (13) and from which the kinetic parameters  $k_1$ ,  $k_2$ , and the ratio  $\alpha_I/\alpha_D$  were determined. The algorithm requires initial estimated values of these parameters for iteration purposes and they where obtained from the limiting cases of eq. (4) for both short and log times. For relatively long operating times, and by assuming that  $k_1 \gg k_2$ , Eq. (13) can be expressed as:

$$\ln\left(\frac{Abs_t}{Abs_0}\right) = \ln\left(\frac{\alpha_I}{\alpha_D k_2}\right) - k_2 t \tag{14}$$

The data in Figure 4a for sonication times larger than 50 min were fitted to Equation (14) by least squares and from which the required initial estimates for  $k_2$  and  $\alpha_I/\alpha_D$  were obtained. At short times the exponential terms in Equation (14) were assumed to be described by the first two terms of the series expansion  $(e^{-ax} \approx 1-ax)$  and after rearrangement yields Equation (15), which permits the calculation of a first estimate of the value of  $k_1$ .

$$k_{1} = \frac{1 - \alpha_{I} / (k_{2} \alpha_{D}) - Abs_{t} / Abs_{0}}{t (1 + \alpha_{I} / (k_{2} \alpha_{D}))}$$
(15)

The obtained values for  $k_1$  and  $k_2$  with their respective 95 percent confidence limits, and the coefficient of determination  $\mathbb{R}^2$  are presented in Table 1.



Fig. 4. Sonolytic color removal kinetic modelling: (a) plot suggesting a two-first order in-series reaction model and (b) model fitted to the experimental data.

Figure 4b shows both sonolytic experimental data and model predictions according to eq. (13), and from which it appears that the scheme accounting for the two first-order in-series reactions can satisfactorily fit the experimental data. It is evident from Table 1 that the reaction rate constant for original dye degradation is much larger than the corresponding one for the intermediates degradation  $(k_1/k_2 = 319)$ . As was observed above for sonolysis degradation (Fig. 4a), two regions were also identified for both the degradation data for the sonolysis system in the presence of Titania particles as well as for the sonophotocatalytic system (see Figs. 5a and c). Therefore, the proposed scheme was assumed in each case and the respective data fitted to eq. (13). The obtained kinetic constants are presented in Table 1 and the experimental data model predictions are shown in Figs. 5b and d.

System	$k_1 (\min^{-1})$	$k_2 (\min^{-1})$	$k_{1}/k_{2}$	R <sup>2</sup>
Sonolysis	$3.100 \times 10^{-2} \pm 0.620 \times 10^{-2}$	$9.717 \times 10^{-5} \pm 0.916 \times 10^{-5}$	319	0.999996
Sonocatalysis	$5.343 \times 10^{-2} \pm 1.631 \times 10^{-2}$	$3.135 \times 10^{-4} \pm 0.309 \times 10^{-4}$	170	0.999896
Sonophotocatalysis	$5.968 \times 10^{-2} \pm 3.853 \times 10^{-2}$	$8.760 \times 10^{-4} \pm 0.609 \times 10^{-4}$	68	0.999891
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	• Experimental — Model	(c) 0 -0.05 -0.15 -0.25 -0.25 -0.25 -0.25 -0.25 -0.25 -0.25 -0.25 -0.25 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.50 -0.00 -0.100 -0.05 -0.25 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.25 -0.3 -0.45	200 25 nin)	50 300
0 50	Time (min)	0 50 100 150 Time (mi	200 25 in)	500 500

Table 1. Kinetic constants for ultrasound in the absence of catalyst, in the presence of catalyst, and in the presence of catalyst in combination with UV light radiation.

Fig. 5. Plot suggesting a two-first order in-series reaction model (a, c), and model fitted to the experimental data (b, d) for sonocatalytic and sonophotocatalytic colour removal kinetic modelling, respectively.

It is clear from Figure 5 that the proposed model is not only able to adequately represent the degradation data of Rhodamine B by sonocatalysis but also the corresponding degradation data by sonophotocatalysis. In both of these cases  $k_1$  was found to be much larger than  $k_2$ , however when considering the three systems presented in Table 1 the relative importance between both reaction rates in terms of the ratio  $k_1/k_2$  was found to be largest for sonolysis, somewhat lower for sonocatalysis, and the smallest for sonophotocatalysis. Albeit the apparent variations in  $k_1/k_2$ , the  $k_1$  values reported in Table 1 for the three systems considered appear not to be statistically different between each other (95% confidence limit). For the case of  $k_2$ , however, significant differences were observed among the three operating modes considered, and it was the sonophotocatalytic system which showed the relatively largest  $k_2$  value. This means that the intermediates are degraded faster using the three methods and the degradation of the dye is carried out with the same speed, independently of the method. In comparison with sonolytic degradation, the additional presence of titania particles (sonocatalysis) and, more significantly the combined operation of ultrasound with titania catalyst and UV radiation (sonophotocatalysis), not only can increase the total color degradation but also seem to promote the degradation rates of the intermediate products.

#### 3.3 Color degradation and mineralization

Dye degradation produces color and colorless products, as well as mineralized material. The

extent of colorless and mineralized products as a function of degradation time was determined for sonophotocatalytic operation by measuring the Total Organic Carbon (TOC) during the process. Three lumps were assumed for the analysis: one expressed as dyes, which comprises color materials ( $C_{LD}$ ); a second lump that includes all intermediate colorless products, ( $C_{LI}$ ); and a third lump for mineralization products ( $C_{LM}$ ). Lump concentrations were expressed in terms of carbon concentrations, and were calculated as follows:

$$C_{LM} = C_{LDo} - C_{TOC} \tag{16}$$

$$C_{LI} = C_{TOC} - C_{LD} \tag{17}$$

where  $C_{LDo}$  stands for the initial dyes carbon concentration and  $C_{TOC}$  refers to the measured TOC concentration at a given reaction time.  $C_{LD}$ is obtained from  $C_{Dye}$  (mgDye L<sup>-1</sup>), determined by spectrophotometry, converted into carbon concentration by eq. (18), where  $m_C$  and  $m_{Dye}$  stand respectively for the weight of carbon in the dye molecule and for the dye molar weight.

$$C_{LD} = \frac{m_C}{m_{Dye}} C_{Dye} \tag{18}$$

Figure 6 presents the calculated dimensionless concentrations for intermediate colorless and mineralized product as calculated from eqs. (16) and (17) for sonophotocatalytic degradation of RhB  $(C_{Li}/C_{LDo})$ . It appears that dyes degrade mainly into colorless products and that mineralized product such as CO<sub>2</sub> represent a comparatively smaller proportion for most of the experiment. It is also apparent in Fig. 6 that the concentration of colorless compounds reaches a maximum concentration after approximately 3 h of reaction, and that it tends to decline afterwards. Mineralized products concentration on the other hand augments slightly but continuously and seems to benefit from the increase of intermediate products degradation mentioned above. From these results it appears that intermediate color products are degraded mainly into colorless soluble products that are subsequently mineralized. Also shown in Fig. 6 is the total carbon concentration present in both colorless and mineralized products  $(C_{LI} + C_{LM})$  and the corresponding calculated values based on the fitted model (eqs. (11)-(13)).



Fig. 6. Concentration profiles for colorless and mineralized intermediate products under sonophotocatalytic RhB dye degradation.

#### Conclusions

The degradation of Rhodamine B by solonolysis, photocatalysis sonocatalysis, and photolysis, sonophotocatalysis has been studied. It appears that degradation by sonolysis increases by the presence of TiO<sub>2</sub> particles and to further augment by sonophotocatalysis. Similarly, while photocatalysis improved photolysis degradation, sonophotocatalysis showed better performance. It appears for both sonolysis and photolysis that the presence of catalyst particles and the combined ultrasound-UV light operation can improve degradation rates by favoring the production of OH radicals, however, a synergetic effect from the dispersion of catalyst particle aggregates, cannot be discarded.

A two first-order in-series reactions model satisfactorily described color degradation under ultrasound, sonocatalysis, and sonophotocatalysis. In all three cases the dye degradation rate into color intermediates  $(k_1)$  was much faster than the degradation rate of the latter into colorless products  $(k_2)$ . However, when compared with ultrasound operation, the magnitude of the kinetic constants for the degradation reactions of color intermediates appears to be the most favored by the presence of catalyst and by combined ultrasound-UV operation  $(k_2 \text{ showed a tenfold increase while } k_1 \text{ doubled its}$ magnitude). Regarding colorless products, they could be either as soluble or mineralized products. It was found that for the sonophotocatalysis process colorless products corresponded mainly to soluble products, which appeared to accumulate in solution and reach a maximum concentration before decreasing in favor of mineralized products.

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